

Additive Manufacturing of Metals and Alloys

3.2 Heat flow in the material and processing maps

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Outline

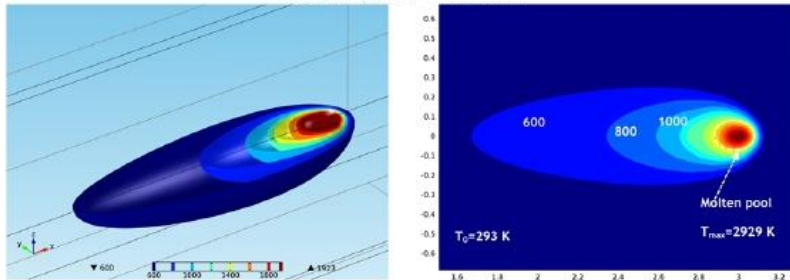
- Thermal history
- Heat flow at the melt pool scale
- Processing maps
- Heat flow : a multiscale problem
- Size effects

Thermal history

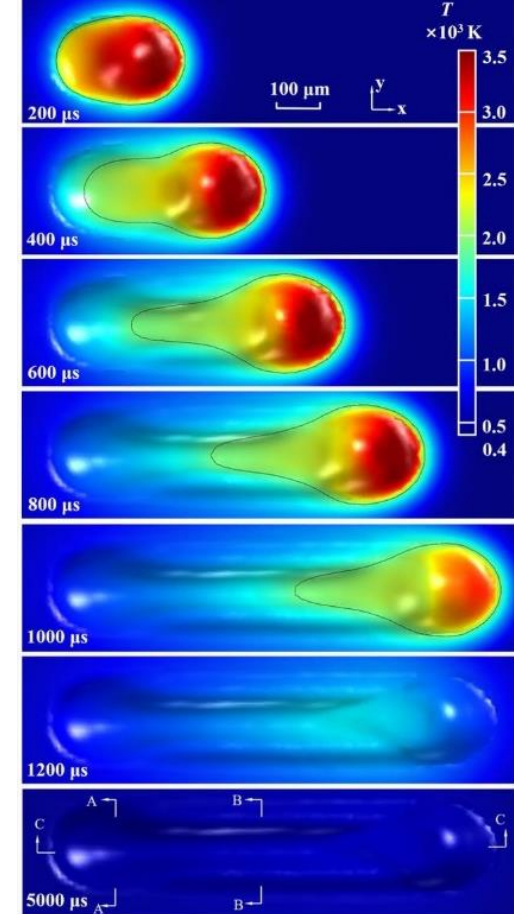
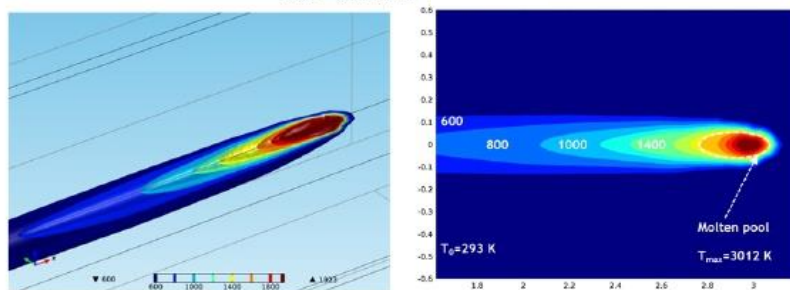
Melt pool morphology

The melt pool is elongated, with a high aspect ratio.

Laser power 50 W, scanning speed 0.1 m/s
13.0 kW/mm²



Laser power 150 W, scanning speed 1.0 m/s
19.1 kW/mm²

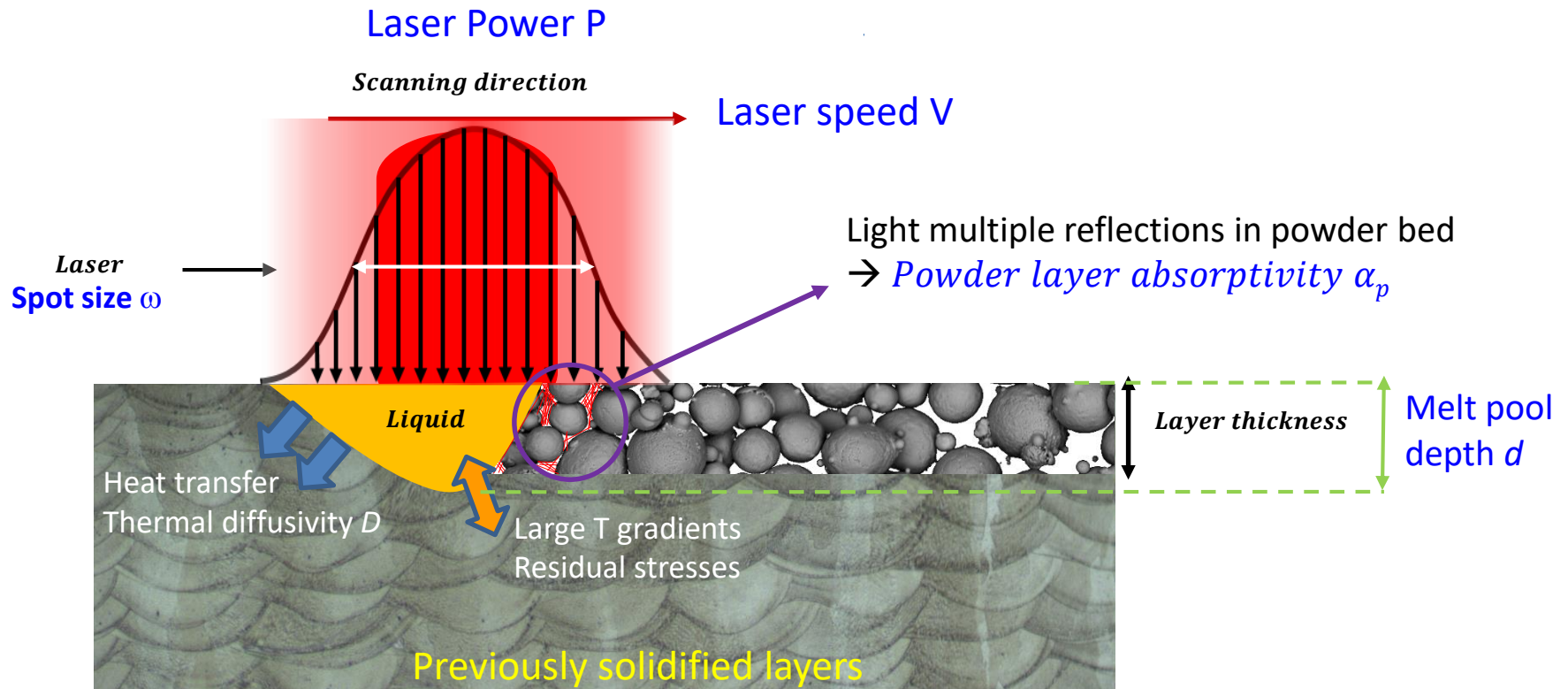


The melt-pool dimensions and morphology are related to:

- the **process parameters** (scanning speed, laser power...)
- the **material** and powder **properties** (thermal conductivity, packing density...)

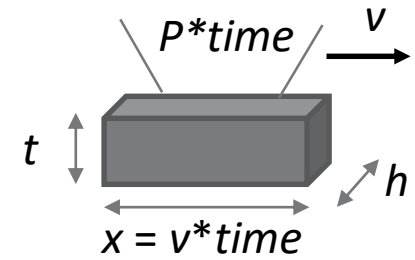
Heat flow in LPBF

Schematic view of the LPBF process at the melt pool scale



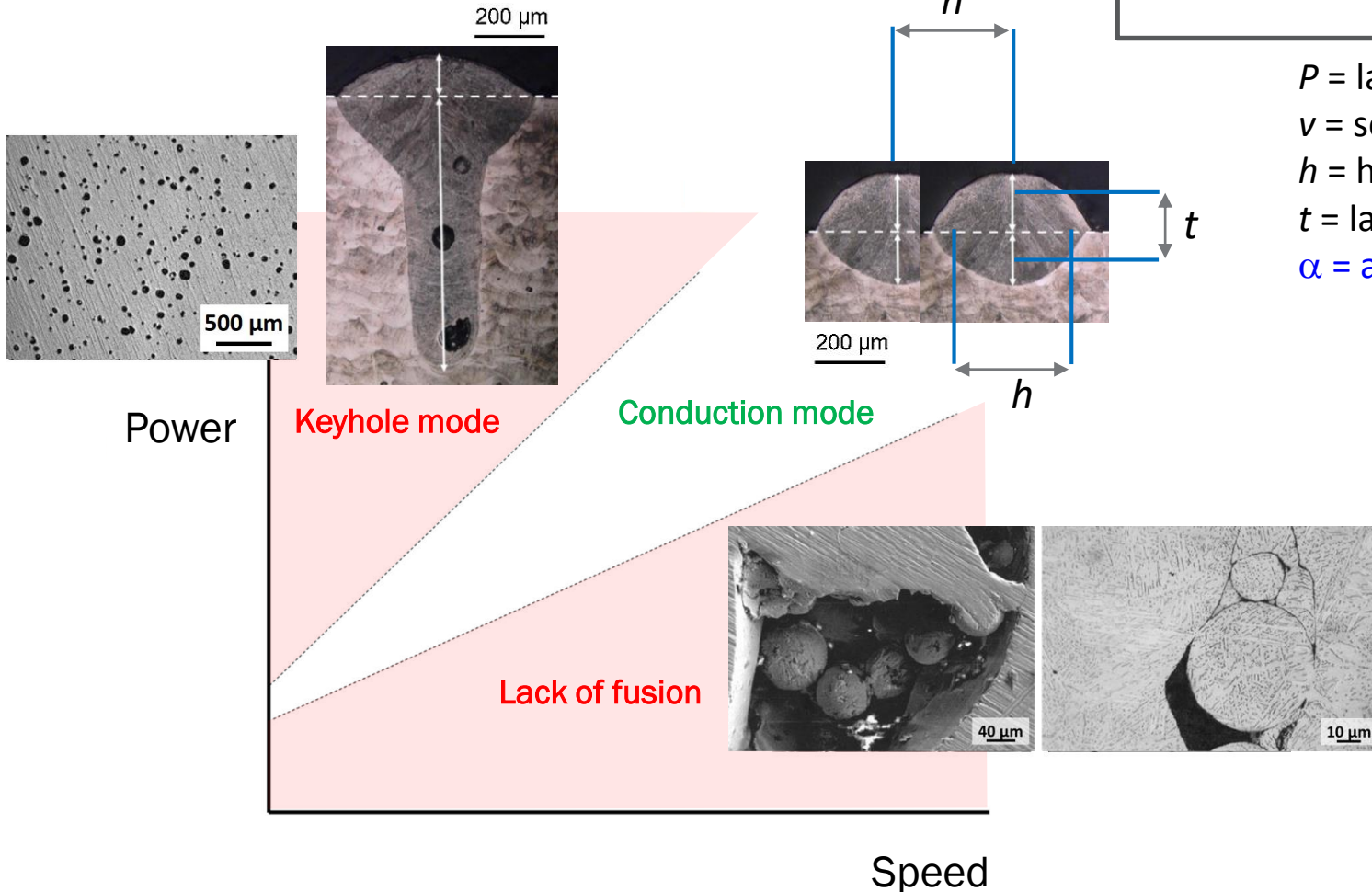
Porosity: processing map

Process window for high density



$$\text{Energy density: } E = \frac{\alpha P}{v h t}$$

P = laser power
 v = scanning speed
 h = hatching distance
 t = layer thickness
 α = absorptivity



Porosity: processing map

Normalized enthalpy vs normalized melt pool depth

Increase in enthalpy
(laser input)

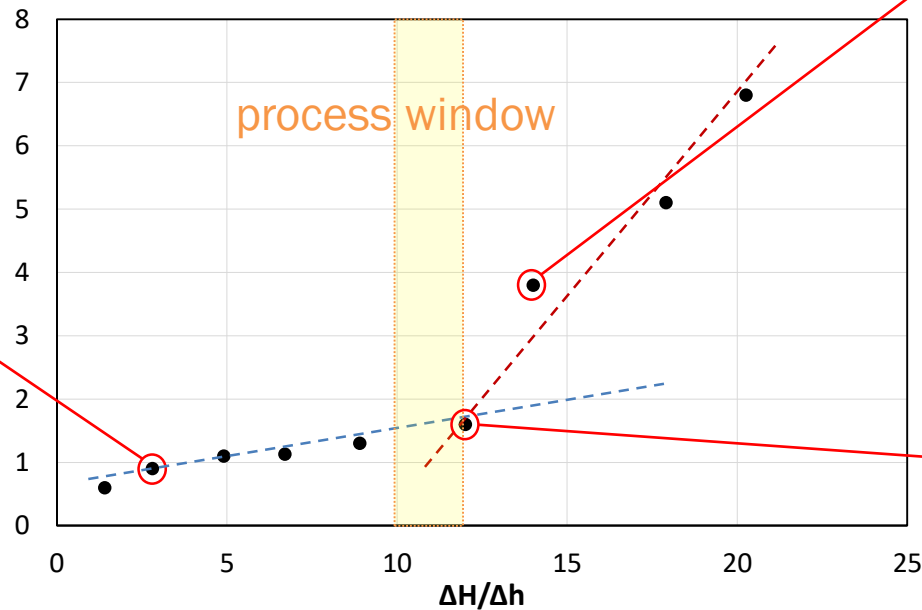
$$\Delta H = \frac{\alpha_p P}{\sqrt{\pi} \omega^3 \sqrt{VD}}$$

Melting enthalpy

$$\Delta h = \rho(C_p \Delta T + L_m)$$

$$\overline{\Delta H} = \frac{\Delta H}{\Delta h}$$

Melt pool depth d / spot size ω



Lack of fusion (LoF)

Deep melt pool and
keyhole pores

No keyhole, no LoF
Conduction mode

⇒ The process window is often narrow

Porosity: processing map

Is the processing map universal?

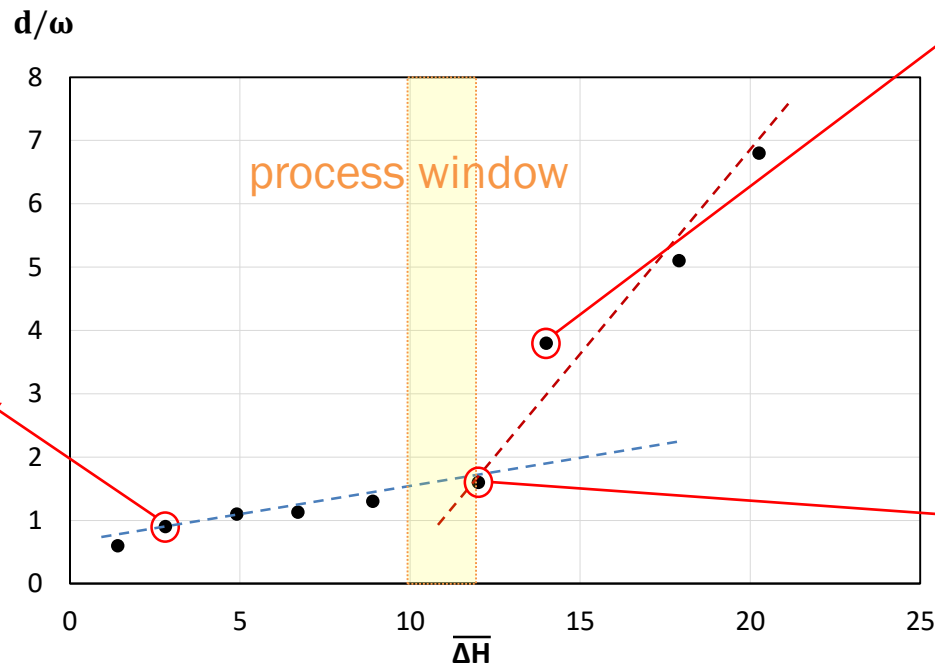
$$\overline{\Delta H} = \alpha_p M \frac{P}{\sqrt{\omega^3 V}}$$

Powder layer
absorptivity

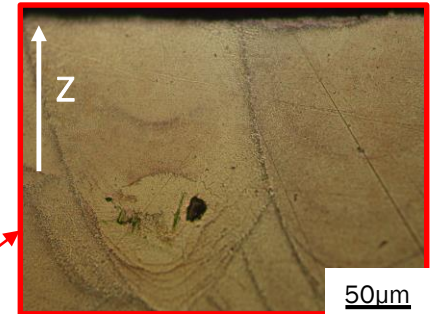
Process parameter

$$M = \frac{1}{\rho(C_p \Delta T + L_m) \sqrt{\pi D}}$$

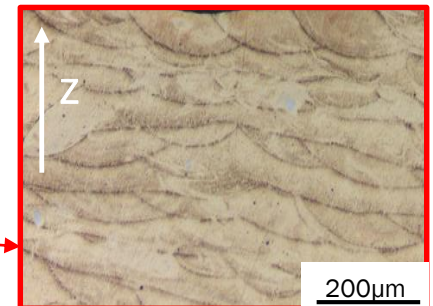
Material parameter



Lack of fusion (LoF)



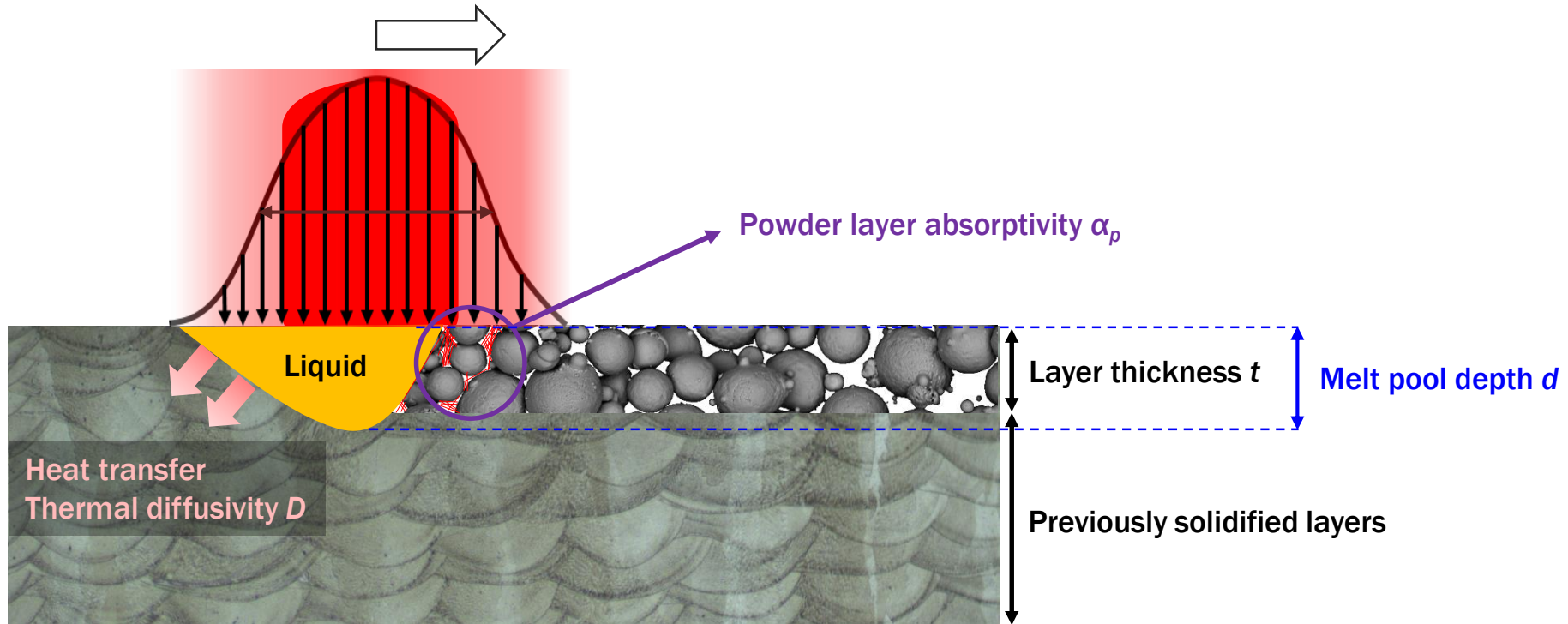
Deep melt pool and
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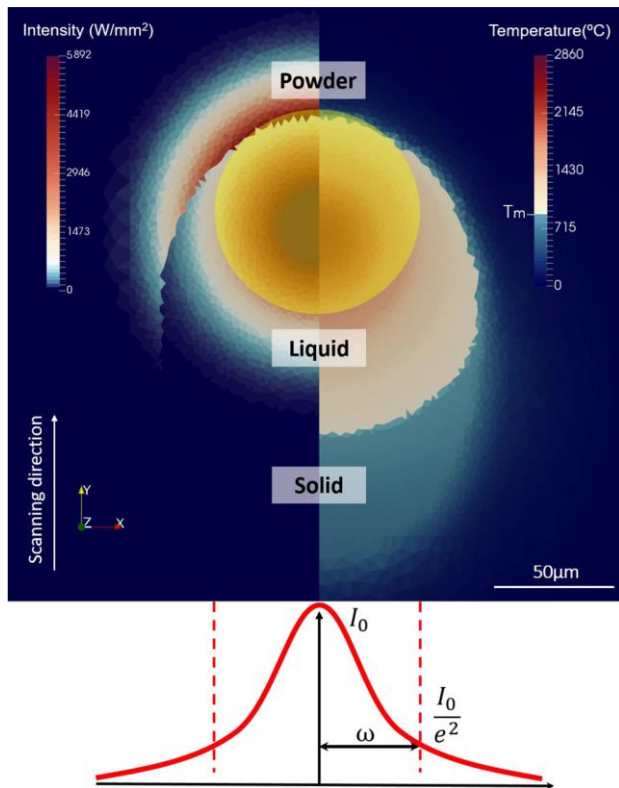
Porosity: processing map

Powder vs liquid absorptivity?



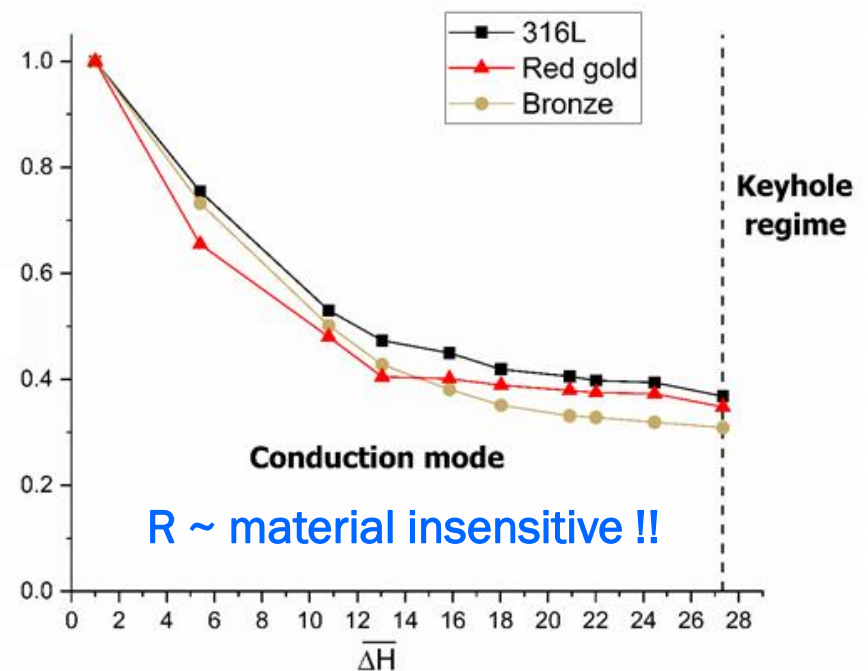
Porosity: processing map

Finite element calculations and translation rule



The optimal normalized enthalpy is a unique reference value for most materials

$$R = \frac{\text{Average absorptivity}}{\text{Powder layer absorptivity}}$$

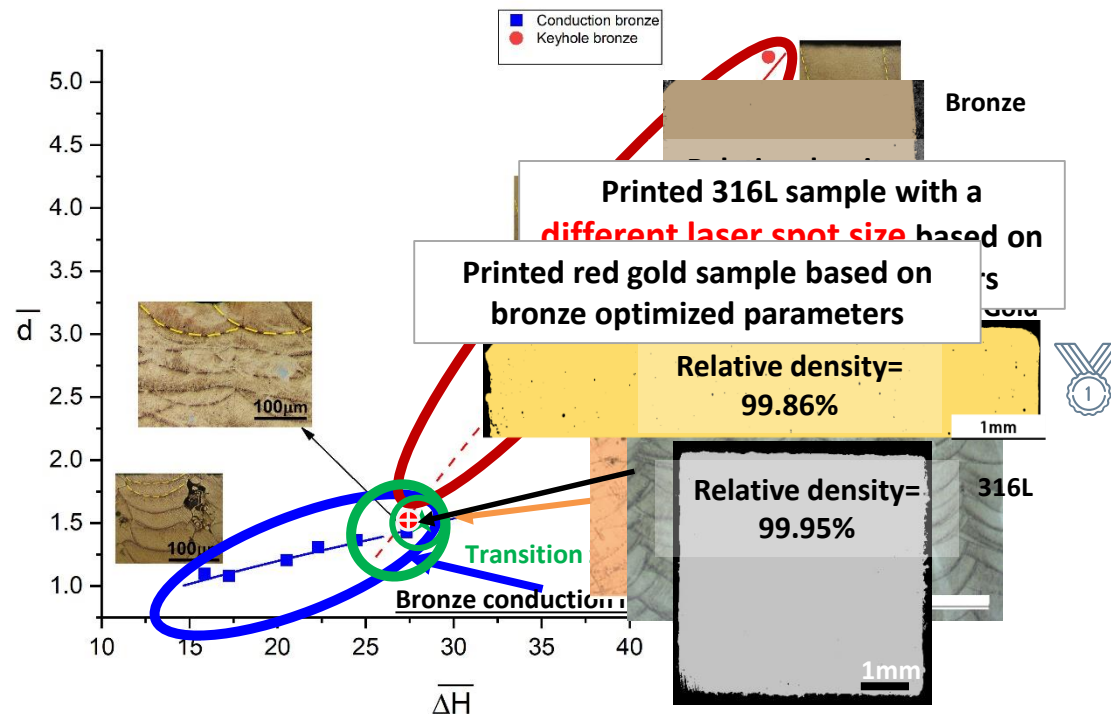


Translation rule : material B $\rightarrow$ material A

$$\left(\frac{P}{\sqrt{\omega^3 V}}\right)_A^{\text{opt}} = \left(\frac{\alpha_p^B}{\alpha_p^A}\right) \cdot \left(\frac{P}{\sqrt{\omega^3 V}}\right)_B^{\text{opt}} \frac{M^B}{M^A}$$

Porosity: processing map

Predicting optimal LPBF conditions for red gold and stainless steel, based on bronze data



Porosity: processing map

Normalized enthalpy vs normalized melt pool depth

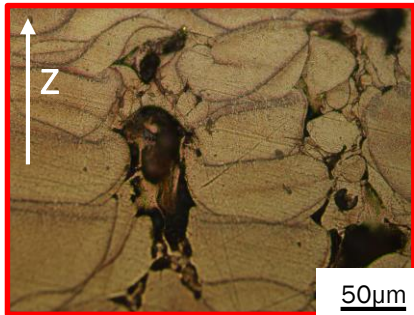
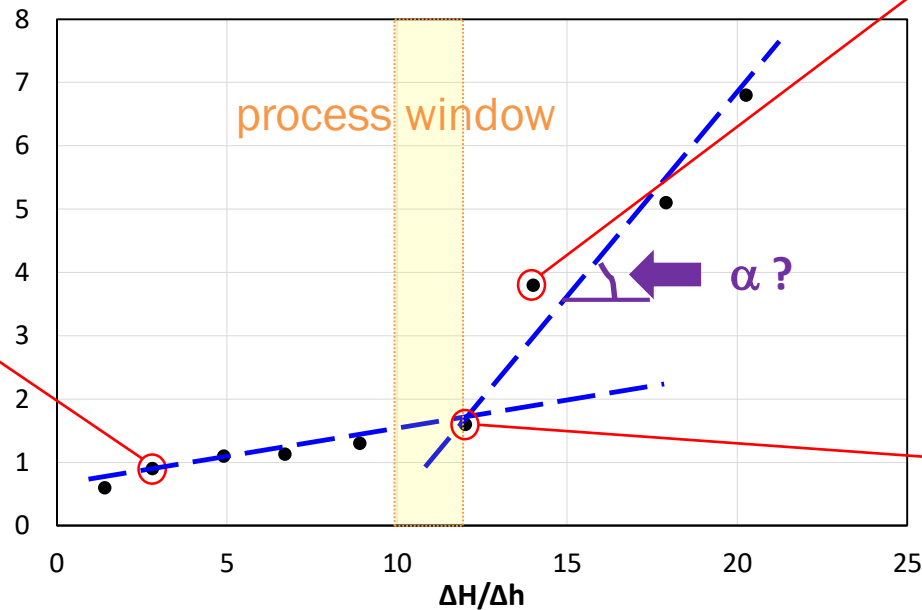
Increase in enthalpy
(laser input)

$$\Delta H = \frac{\alpha_p P}{\sqrt{\pi \omega^3 V D}}$$

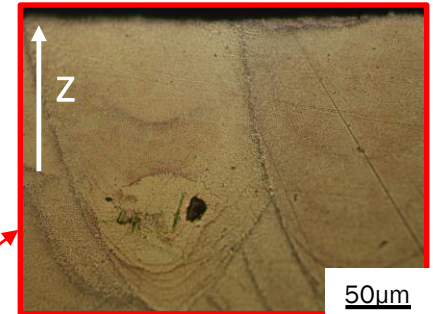
Melting enthalpy

$$\Delta h = \rho(C_p \Delta T + L_m)$$

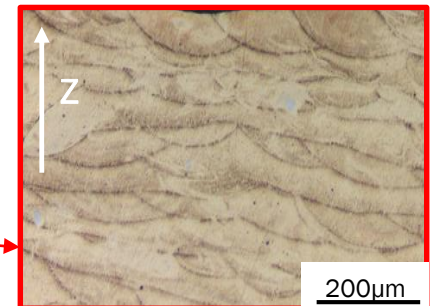
Melt pool depth d / spot size ω



Lack of fusion (LoF)



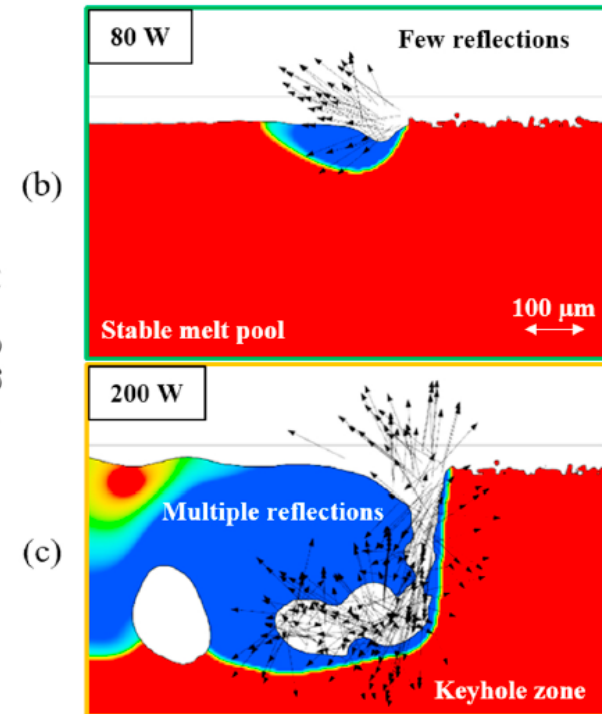
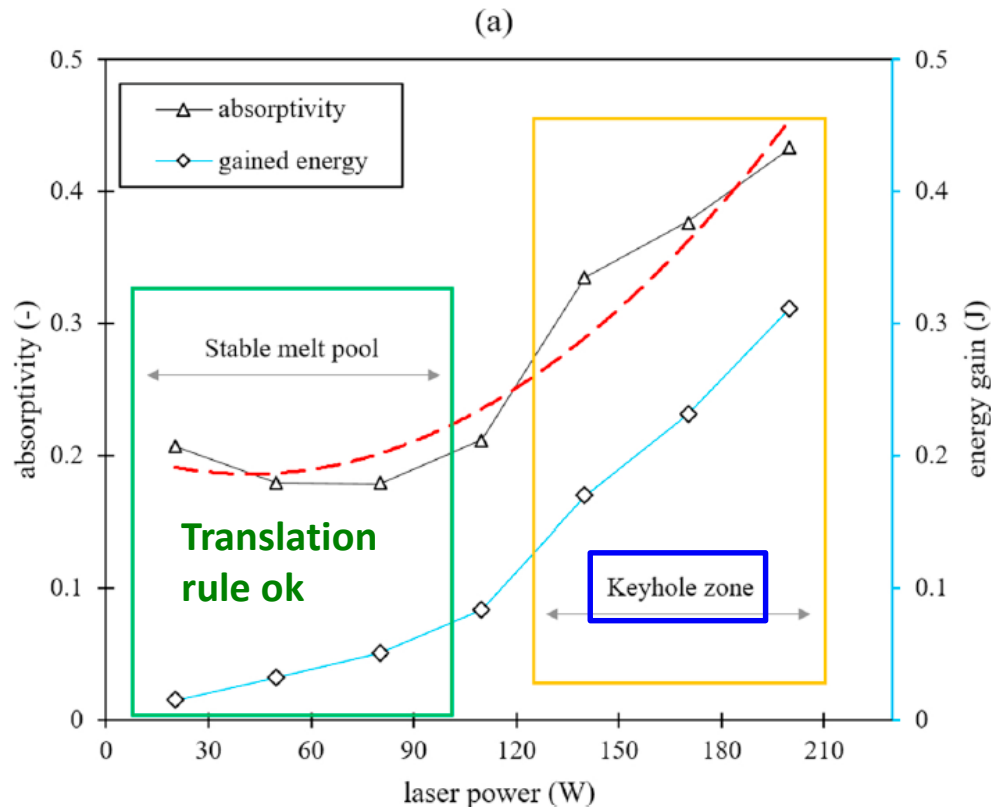
Deep melt pool and
keyhole pores



No keyhole, no LoF
Conduction mode

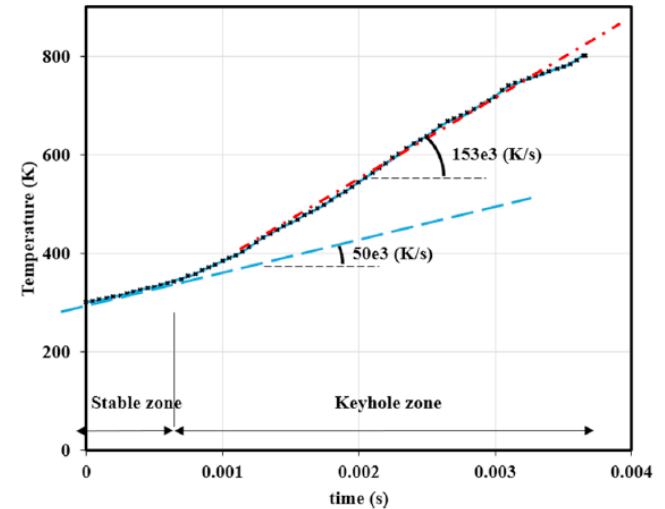
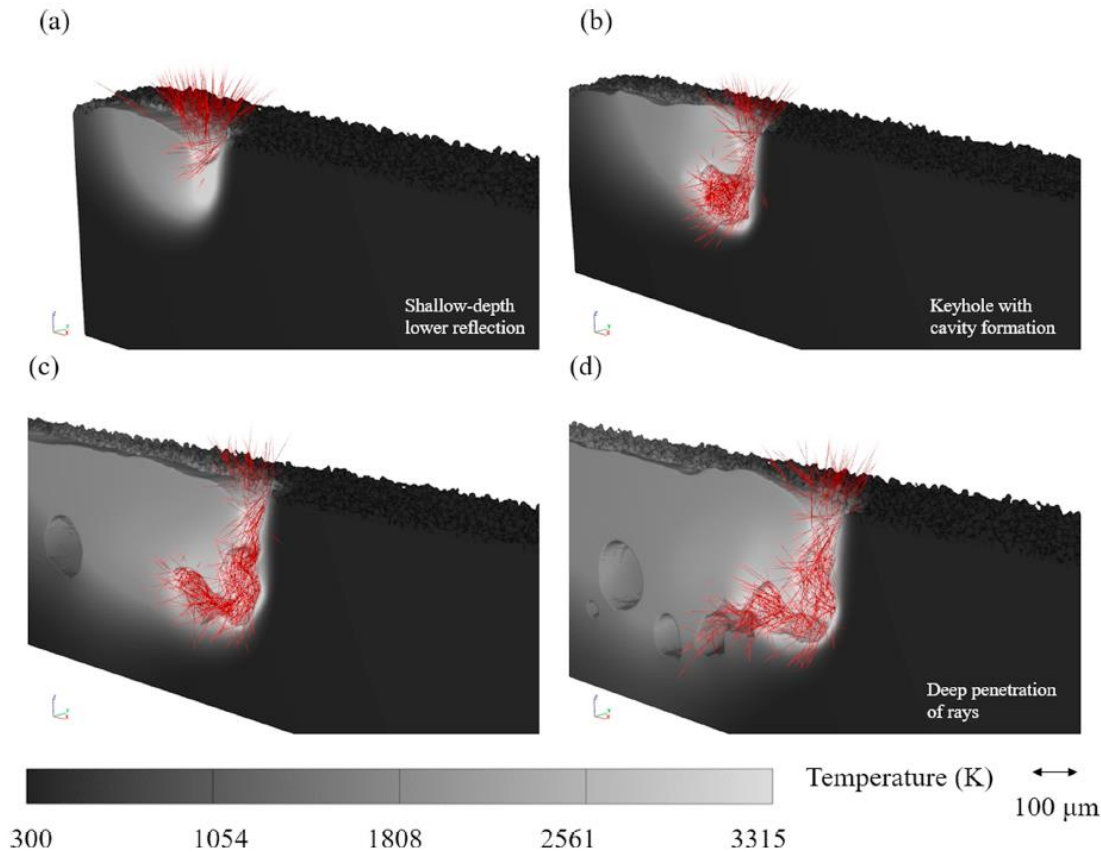
⇒ The process window is often narrow

Absorptivity as a function of processing regime



M. Bayat, A. Thanki, S. Mohanty, A. Witvrouw, S. Yang, J. Thorborg, N. Skat Tiedje, J. Henri Hattel, Keyhole-induced porosities in Laser-based Powder Bed Fusion (L-PBF) of Ti6Al4V: High-fidelity modelling and experimental validation, Additive Manufacturing 30 (2019), 100835, <https://doi.org/10.1016/j.addma.2019.100835>

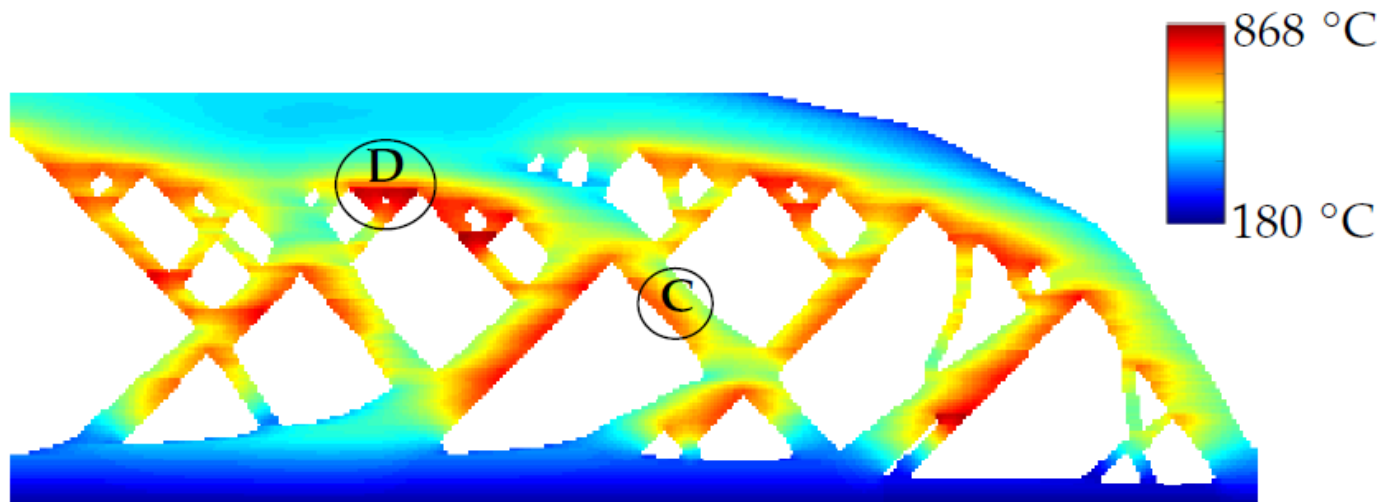
Absorptivity and energy absorption



M. Bayat, A. Thanki, S. Mohanty, A. Witvrouw, S. Yang, J. Thorborg, N. Skat Tiedje, J. Henri Hattel, Keyhole-induced porosities in Laser-based Powder Bed Fusion (L-PBF) of Ti6Al4V: High-fidelity modelling and experimental validation, Additive Manufacturing 30 (2019), 100835, <https://doi.org/10.1016/j.addma.2019.100835>

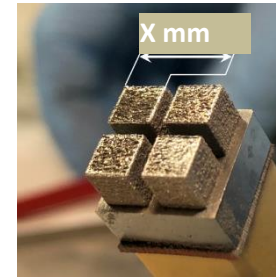
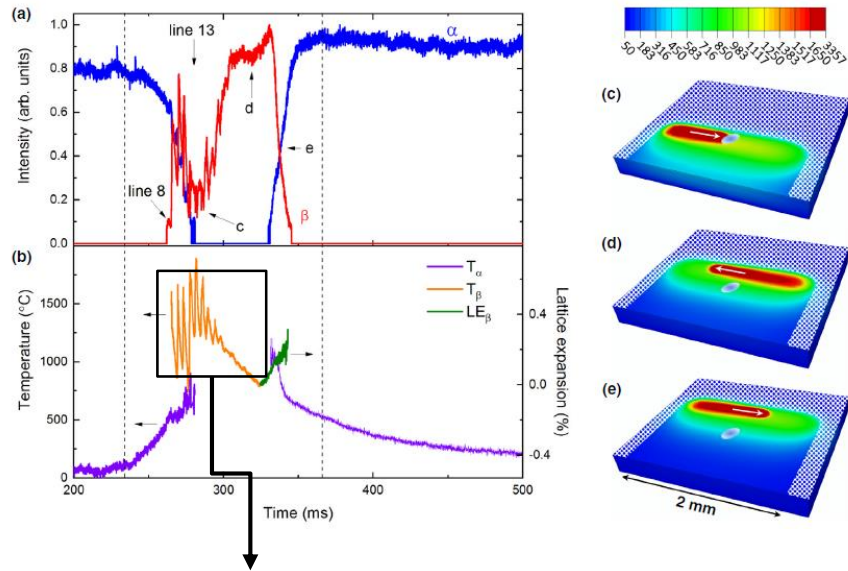
Heat flow in LPBF : a multiscale problem

Schematic view of maximum T reached at the **part scale**



Contour plot of maximum temperature attained during the entire build simulation. Region D shows higher maximum temperatures than Region C.

Size effects

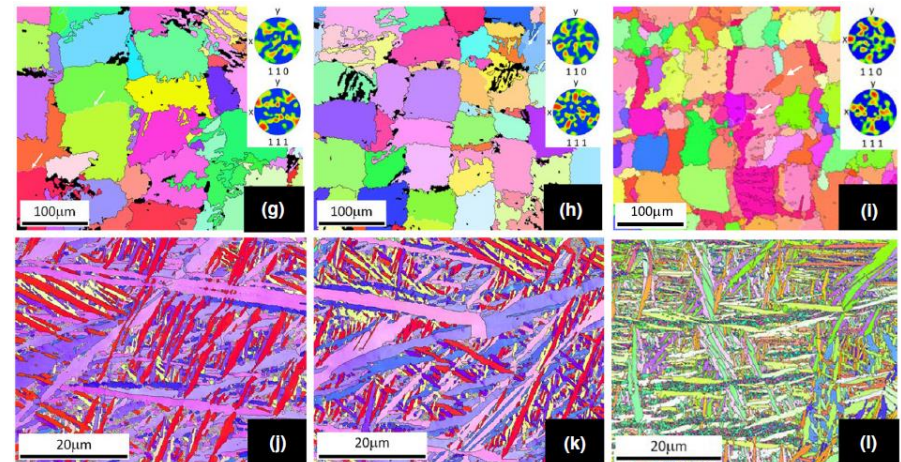


Ti-6Al-4V

X = 2 mm

X = 4 mm

X = 6 mm



Depending on the value of X (sample dimension), the temperatures reached in samples change:

- β phase lasts **7 ms** for x= **6 mm** scanning vector
- β phase lasts **84 ms** for x= **2 mm** scanning vector

(β = high temperature phase in Ti-6Al-4V)

S. Hocine, H. Van Swygenhoven, S. Van Petegem, C. Sin Ting Chang, T. Maimaitiyili, G. Tinti, D. Ferreira Sanchez, D. Grolimund, N. Casati, Operando X-ray diffraction during laser 3D printing, Materials Today 34 (2020), 30-40, <https://doi.org/10.1016/j.mattod.2019.10.001>

(See chapter on microstructure control through processing)

References

- H. Ghasemi-Tabasi, J. Jhabvala, E. Boillat, T. Ivas, R. Drissi-Daoudi, R. E. Logé (2020), An effective rule for translating optimal selective laser melting processing parameters from one material to another, *Additive Manufacturing* 36, 101496. <https://doi.org/10.1016/j.addma.2020.101496>
- S. Hocine, H. Van Swygenhoven, S. Van Petegem, C. Sin Ting Chang, T. Maimaitiyili, G. Tinti, D. Ferreira Sanchez, D. Grolimund, N. Casati, Operando X-ray diffraction during laser 3D printing, *Materials Today* 34 (2020), 30-40. <https://doi.org/10.1016/j.mattod.2019.10.001>
- M. Bayat, A. Thanki, S. Mohanty, A. Witvrouw, S. Yang, J. Thorborg, N. Skat Tiedje, J. Henri Hattel, Keyhole-induced porosities in Laser-based Powder Bed Fusion (L-PBF) of Ti6Al4V: High-fidelity modelling and experimental validation, *Additive Manufacturing* 30 (2019), 100835, <https://doi.org/10.1016/j.addma.2019.100835>
- Ranjan, R.; Ayas, C.; Langelaar, M.; van Keulen, F. Fast Detection of Heat Accumulation in Powder Bed Fusion Using Computationally Efficient Thermal Models. *Materials* **2020**, *13*, 4576. <https://doi.org/10.3390/ma13204576>
- Additive Manufacturing: Materials, Processes, Quantifications and Applications, edited by Jing Zhang and Yeon-Gil Jung, Butterworth-Heinemann, 2018.